

ENP100 - Proses og produksjon

Øving 9 - Løsningsforslag

Opgave 1:

$$a) \text{ Oppgitt: } \begin{cases} \dot{m} u = \frac{\dot{m}}{A} \\ \rho = \frac{P}{ZRT} \end{cases} \left(\begin{array}{l} \text{Fordi massestrøm, } \dot{m} \text{ [kg/s]} \\ = u \cdot A \cdot \rho \quad \text{kg/m}^3 \\ \frac{\text{m}}{\text{s}} \cdot \text{m}^2 = \frac{\text{m}^3}{\text{s}} \text{ (= Volumstrøm)} \end{array} \right)$$

$$\downarrow \left(\begin{array}{l} \text{Fordi reell gass: } p v = ZRT; \quad \rho = \frac{1}{v} \\ \downarrow \\ \text{spesifikt volum} \end{array} \right)$$

$$\text{Trykkløstledd: } -\frac{dp}{dL} = \frac{1}{2} f_0 \cdot \frac{\rho u^2}{D} = \frac{f_0}{2D} \cdot \rho u^2$$

konstant.

$$\text{Skriv så } \rho u^2 = \frac{(\dot{m})^2}{\rho A^2} = \frac{(\dot{m}/A)^2}{P/ZRT} = \frac{\dot{m}^2 ZRT}{P \cdot A^2}$$

$$\text{Satt inn: } -\frac{dp}{dL} = K \cdot \frac{\dot{m}^2 ZRT}{P A^2}$$

$$\text{Løst mhp. } dL: \quad dL = - \frac{A^2}{K \cdot ZRT \cdot \dot{m}^2} p dp$$

QED

b) Integren fra $L=0$ til $L=L$; der med fra $P=P_1$ til $P=P_2$:

$$\int_0^L dL = - \frac{A^2}{K \cdot ZRT \cdot \dot{m}^2} \int_{P_1}^{P_2} p dp \rightarrow L = - \frac{A^2}{K \cdot ZRT \cdot \dot{m}^2} \cdot \frac{1}{2} (P_2^2 - P_1^2)$$

Lös mhp. \dot{m}

(Sinnvoll fortgesetzt bei, wenn $P_1 > P_2$)

$$\dot{m}^2 = \frac{A^2 \cdot (P_1^2 - P_2^2)}{2 \cdot k \cdot ZRT \cdot L} \Rightarrow \dot{m} = \sqrt{\frac{(P_1^2 - P_2^2) \cdot A^2}{2 \cdot k \cdot ZRT \cdot L}}$$

Sett imm fall ; OBS einleiten:

* Gaskonstanten på molar basis:

$$R = \frac{R_0}{M_w}$$

$$R_0 = 8.3144 \frac{\text{J}}{\text{mol K}} \text{ (universell)}$$

$$M_w = \gamma_g \cdot M_{w, \text{luft}} = 0.63 \cdot 29 \frac{\text{g}}{\text{mol}}$$

$$R = \frac{8.3144 \frac{\text{J}}{\text{mol K}}}{0.63 \cdot 29 \frac{\text{g}}{\text{mol}}} = 0.455 \frac{\text{J}}{\text{g K}} = \underline{\underline{455 \frac{\text{J}}{\text{kg K}}}}$$

* Temperatur i K: $T = 7.3^\circ\text{C} + 273.15 = \underline{\underline{280.45\text{K}}}$

$$\dot{m} = \sqrt{\frac{[(137 \cdot 10^5)^2 - (85 \cdot 10^5)^2] \cdot (0.46 \text{ m}^2)^2}{2 \cdot 0.0065 \frac{1}{\text{m}} \cdot 0.94 \cdot 455 \cdot 280.45 \cdot 540000 \text{ m}}}$$

Enhets - sjekke:

$$\frac{\left(\frac{\text{N}}{\text{m}^2}\right)^2 \cdot \text{m}^4}{\frac{1}{\text{m}} \cdot \frac{\text{Nm}}{\text{kg K}} \cdot \text{K} \cdot \text{m}} = \frac{\text{N}^2 \text{ kg}}{\text{Nm}}$$
$$= \frac{\text{kg} \cdot \text{m}}{\text{s}^2} \cdot \frac{\text{kg}}{\text{m}} = \frac{\text{kg}^2}{\text{s}^2}$$

$$\rightarrow \dot{m} = \sqrt{29009 \frac{\text{kg}^2}{\text{s}^2}} = \underline{\underline{170.3 \frac{\text{kg}}{\text{s}}}}$$

c) Weizmann-formulen: Trynge D

$$\rightarrow D = \sqrt{\frac{4A}{\pi}} = \sqrt{\frac{4 \cdot 0.46 \text{ m}^2}{\pi}} = \underline{0.765 \text{ m}} \quad (A=0.46 \text{ m}^2)$$

Til passende enheder:

$$P_1 = 137 \text{ bar} = 13700 \text{ kPa}$$

$$P_2 = 85 \text{ bar} = 8500 \text{ "}$$

(eller "som før")

$$\dot{q}_{sc} = 1.185 \cdot 10^7 \cdot \left(\frac{288.15 \text{ K}}{101.325 \text{ kPa}} \right)^{5.333} \cdot \sqrt{\frac{(13700^2 - 8500^2) \cdot 0.765}{0.63 \cdot 540000 \cdot 280.45 \cdot 0.94}}$$

$$= 18\,716\,427 \frac{\text{Sm}^3}{\text{d}} = \underline{18.72 \cdot 10^6 \frac{\text{Sm}^3}{\text{d}}}$$

d) Må konverteren en an dem;

$$18.72 \cdot 10^6 \frac{\text{Sm}^3}{\text{d}} \cdot 42300 \frac{\text{kmol}}{10^6 \text{Sm}^3} \cdot 0.63 \cdot 29 \frac{\text{kg}}{\text{kmol}} \cdot \frac{1}{86400 \text{ s/d}}$$

$$= \underline{167.4 \frac{\text{kg}}{\text{s}}}$$

$$\rightarrow \frac{167.4 - 170.3}{167.4} \approx -0.017 = \underline{\underline{1.7\%}}$$

Opgave 2:

a) pwf (after the lift gas is introduced) = 2900 psia; the necessary casing pressure at well depth will be 100 psi higher; $p_{c,v} = 3000$ psia

b) Surface casing pressure given by equation (17.8) assumes only hydrostatic pressure difference due to the weight of the gas itself.

$$p_{c,s} = 3000 \cdot e^{-0.01875 \cdot \frac{0.65 \cdot 10000}{0.9 \cdot (95 + 460)}} = \underline{\underline{2350 \text{ psi}}}$$

(The approximation leading up to equation (17.10) is obsolete, since now we do have calculators ...)

c) In simplified analysis like this one usually ignore topside pressure drops in piping:

The compressor should compress the lift gas from pwh = 1450 psia, up to $p_{c,s} = 2350$ psia;

Using the equations from chp. 11, performing the calculations in metric units should be more convenient, as long as we need not worry about the pressure units:

$$R = \frac{8.314 \text{ J/mol K}}{0.65 \cdot 29 \text{ g/mol}} = 0.441 \text{ J/g} = \underline{\underline{441 \text{ J/kg K}}}$$

$$95^\circ \text{F} = 95 + 460 = 555^\circ \text{R} \times \frac{1}{1.8} = \underline{\underline{308 \text{ K}}}$$

$$\rightarrow W_s = \frac{1.24}{0.24} \cdot 441 \cdot 308 \cdot \left[\left(\frac{2350}{1450} \right)^{\frac{0.24}{1.24}} - 1 \right] = 68747 \text{ J/kg}$$

Then convert to US Field:

$$W_s = 68747 \frac{\text{J}}{\text{kg}} \cdot 0.73766 \frac{\text{ft} \cdot \text{lb}_f}{\text{J}} \cdot \frac{1 \text{ kg}}{2.205 \text{ lb}_m} = 22999 \frac{\text{ft} \cdot \text{lb}_f}{\text{lb}_m}$$

Using equation (17.24) directly will give the same result, given some round-off errors:

$$W = \frac{1.24}{0.24} \cdot \frac{53.241 \cdot 555}{0.65} \cdot \left[\left(\frac{2350}{1450} \right)^{\frac{0.24}{1.24}} - 1 \right] = 23009 \frac{\text{ft} \cdot \text{lb}_f}{\text{lb}_m}$$